



superior performance.
powerful technology.

C-axis Tensile Strength of 2G HTS

Yi-Yuan Xie, Brian Liebl, Sofia Soloveichik, Lance Hope, Drew Hazelton, and John Dackow
SuperPower, Inc, Schenectady, NY

Ronald B. Bucinell, Andrew Brown
Union College, Schenectady NY



Venkat Selvamanickam
University of Houston, Houston TX



Applied Superconductivity Conference
August 1-6, 2010 ■ Washington, DC

celebrating
10 years
2000 ~ 2010

PHILIPS

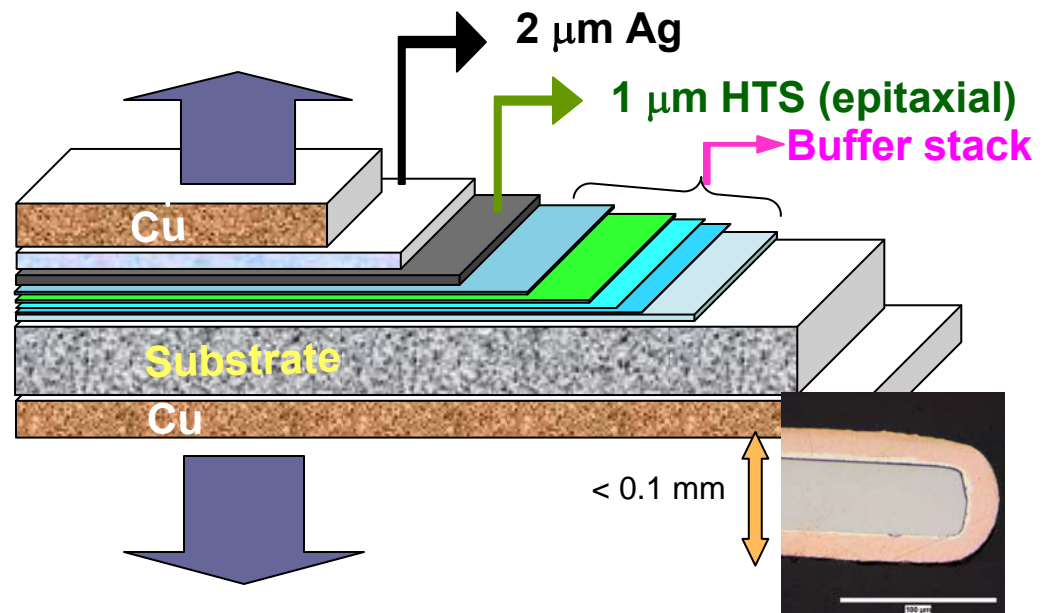
SuperPower, Inc. is a subsidiary of Philips Medical Systems MR, a division of Royal Philips Electronics N.V.

Origin of c-axis tensile stress in large-scale applications

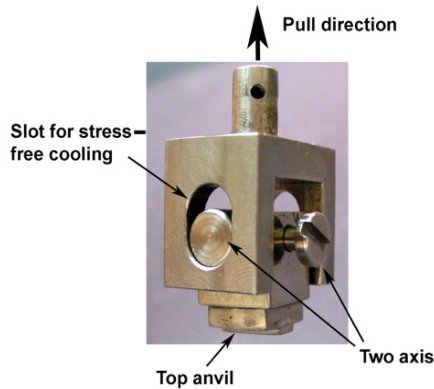
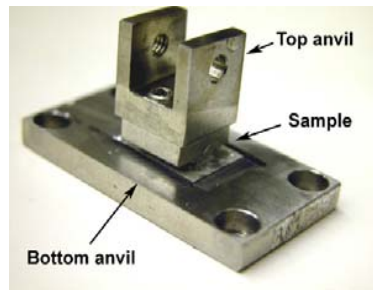
- Among all real-world applications in which 2G HTS wire will be eventually used as the key material to achieve high performance and energy efficiency, coil-based applications require 2G HTS to withstand c-axis tensile stress due to multiple origins:

- Mismatch in thermal expansion: substrate vs. ceramic layer vs. Cu
- Radial forces due current – field interaction
- High-speed rotational forces
- Coil fabrication related reasons

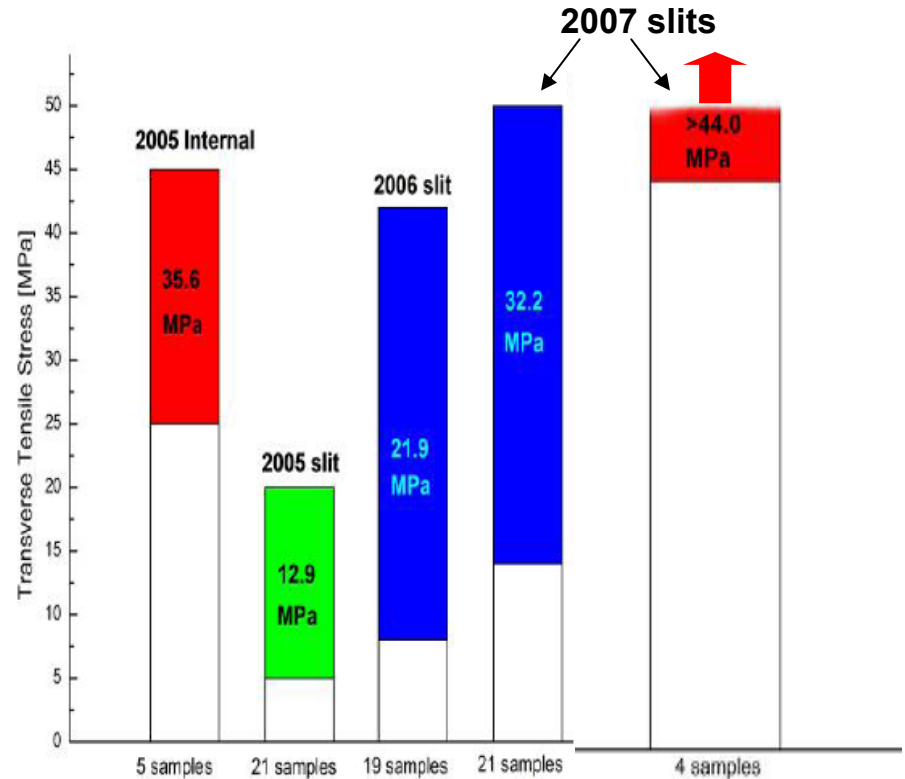
- Those stresses are estimated to be at the level of a few to a few tens of MPa. More accurate modeling needs to be developed



MOCVD/IBAD-MgO based 2G HTS show c-axis tensile strength up to 50+ MPa



N. Cheggour, D. van der Laan, C. Clickner, and J. Ekin
 2007 DOE Peer Review



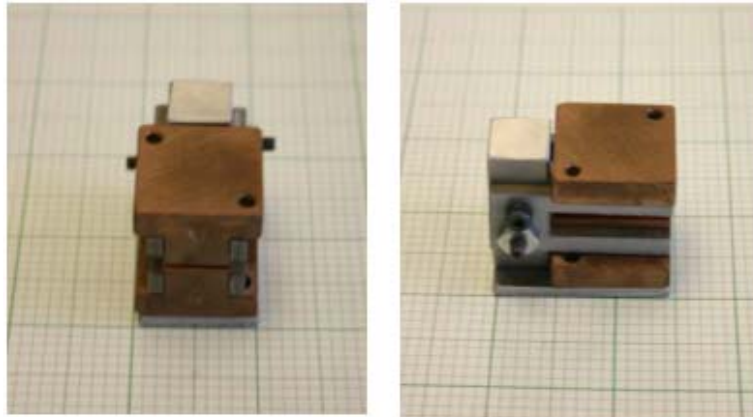
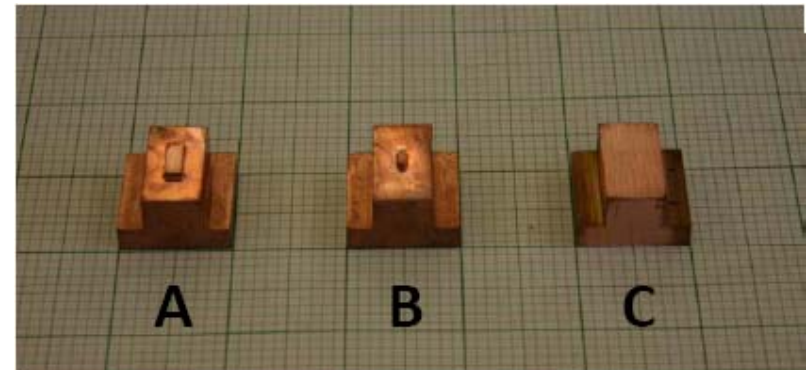
NIST developed a c-axis pulling test method and systematically tested MOCVD/IBAD-MgO based 2G HTS showing year-to-year improvement in c-axis tensile strength:

- High c-axis tensile strength above 50 MPa – bonding in multilayer interfaces can be very strong
- Reason for the spreading in the range from 15 MPa to 50+MPa unclear: error in test or non-uniformity in the conductor?

Alignment fixtures developed and anvil configuration explored to improve reproducibility

Several anvil configurations explored to generate proper failures

- Anvil A: 40 mm²
- Anvil B: 9.14 mm² (HTS)
- Anvil C: 288 mm² (Substrate)

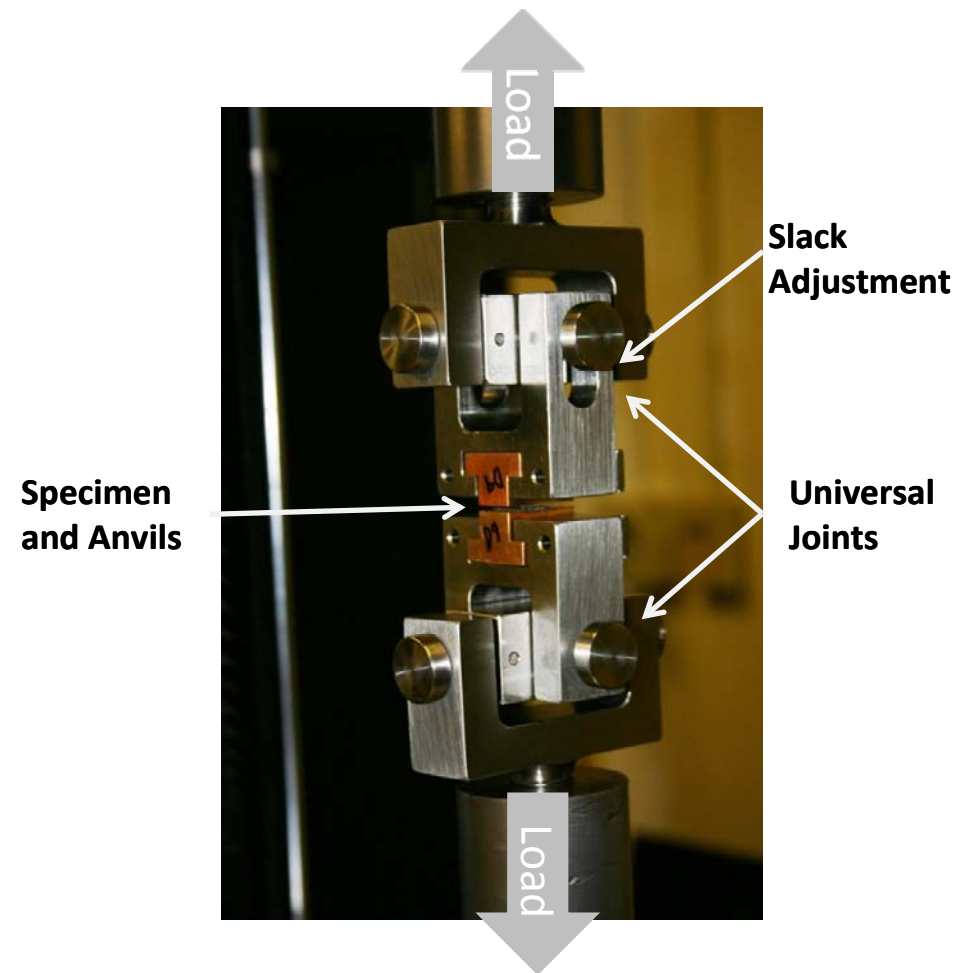


Alignment fixtures developed

- Ensure anvil location on tape
- Ensure anvils are square
- Speeds sample preparation

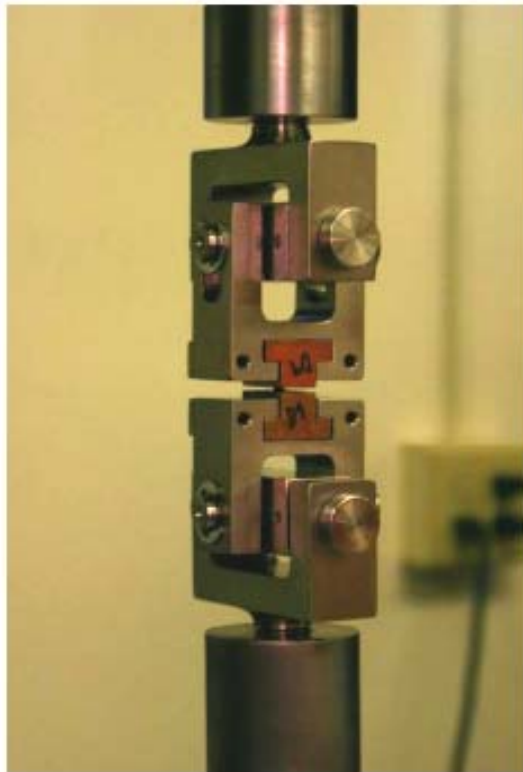
NIST c-axis pulling test method modified to improve performance and ease of use

- Dual universal joints
 - Eliminates all bending
 - Ensures load is only normal to tape adjustment
- Slack adjustment
 - Stress free specimen mounting
- Replaceable specimen anvils
 - Ease of mounting in test fixtures
 - Minimizes disposable parts
 - Simplifies specimen preparation



0.25 mm/min load rate

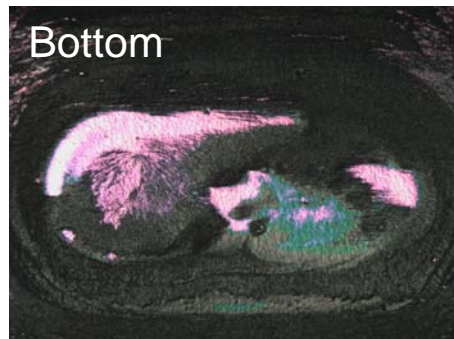
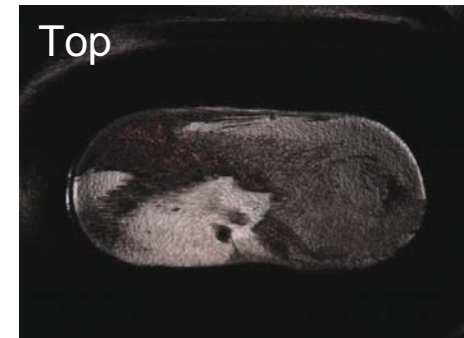
New configuration accommodates testing at room temperature and at 77 K



Room temperature configuration



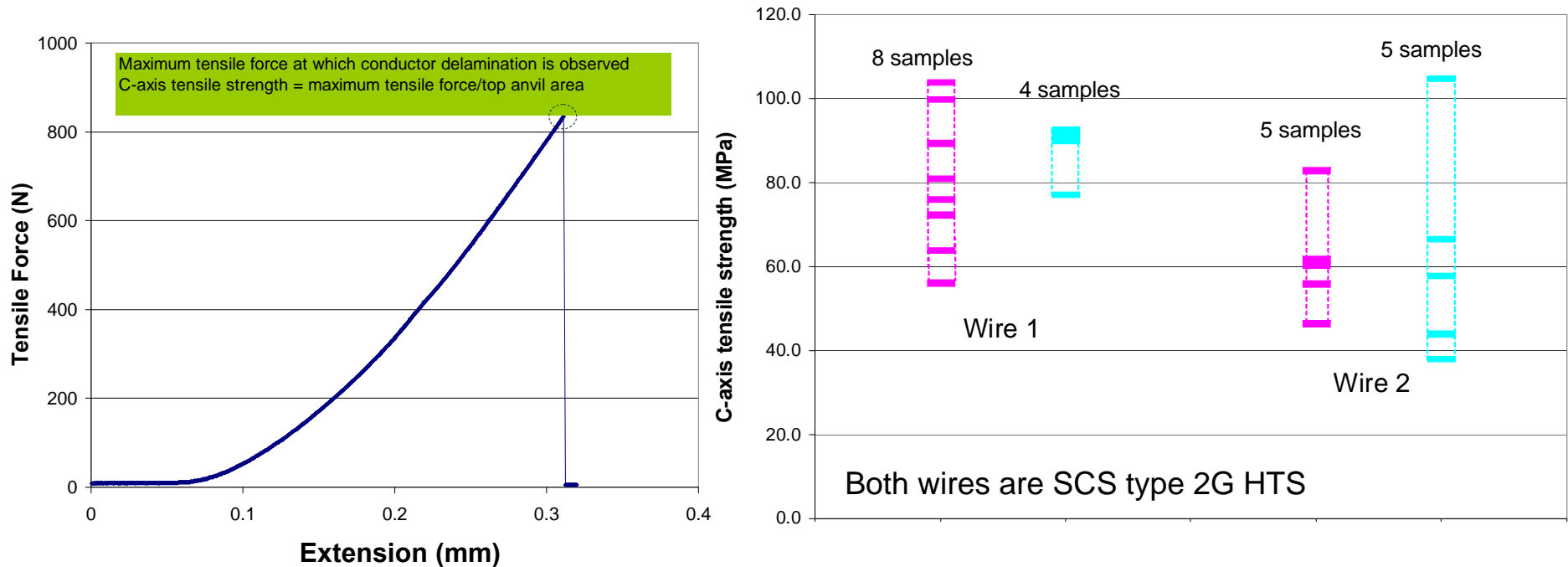
Cryogenic temperature configuration



Typical delamination mode:

- Upper part of the multilayer structure including HTS attached to top anvil
- Lower part of the multilayer structure including substrate attached to bottom anvil

C-axis tensile stress test results by anvil method



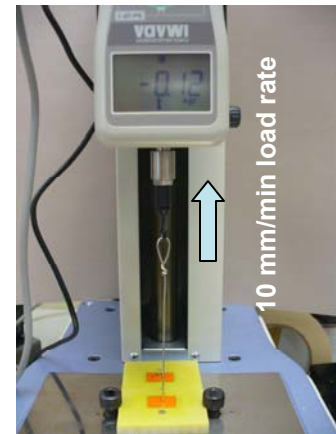
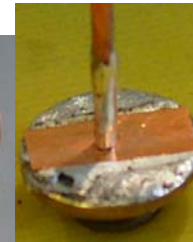
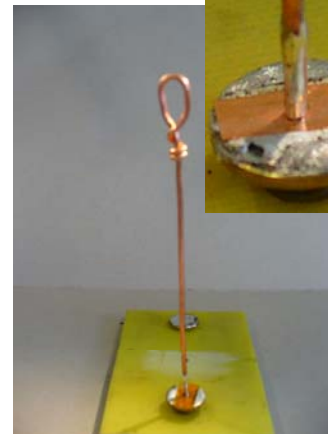
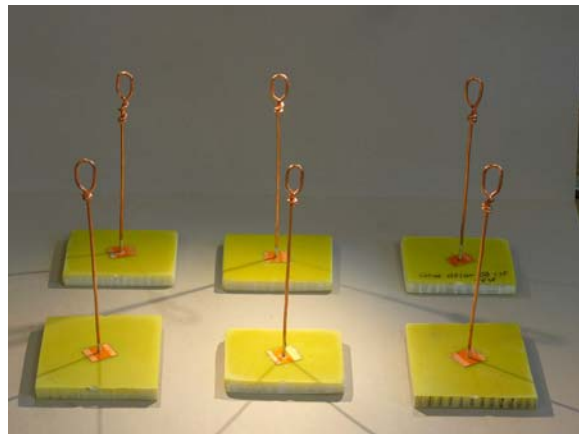
C-axis tensile stress measurement value shows some variation within each wire

- Wire 1: 56 - 104 MPa @ Room Temp, 77-93 MPa at 77 K
- Wire 2: 46 - 83 MPa @ Room temp; 38 - 105 MPa

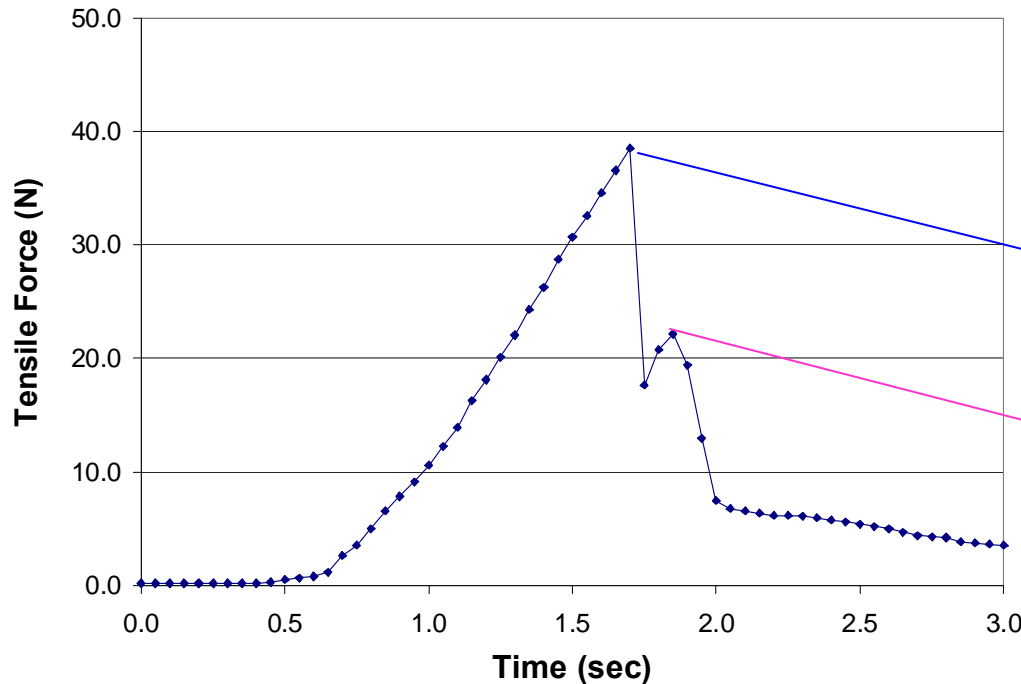
No systematic difference between c-axis stress values at room temp and 77 K

An alternative c-axis tensile test method also developed to measure strength at small regions

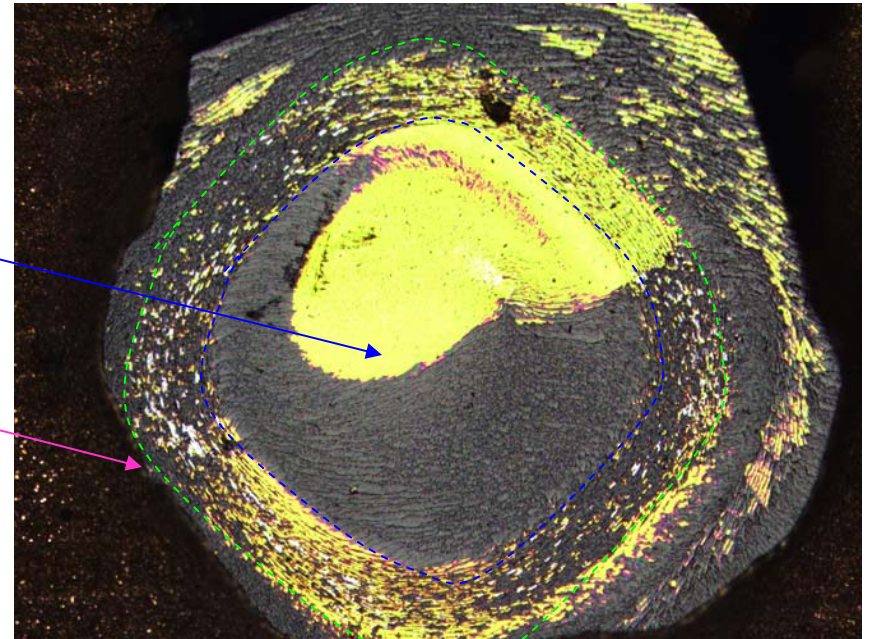
- Solder-pin method - test procedure developed
 - Place a Kapton tape mask with a pre-cut hole in size of about 1-1.5 mm by 1-1.5 mm on the cleaned wire surface. Solder a solder pin in size of 1.5 mm in diameter normal to HTS side of the wire surface, and then glue or solder the substrate side of the wire to a bottom plate.
 - Mount the sample assembly to a commercial tensile tester, applied tensile force, record the load curve and observe the delamination situation
 - Examine the delamination region with OM, record the size of the debond zone and calculate the tensile stress at which conductor delaminates



Test result by solder-pin method



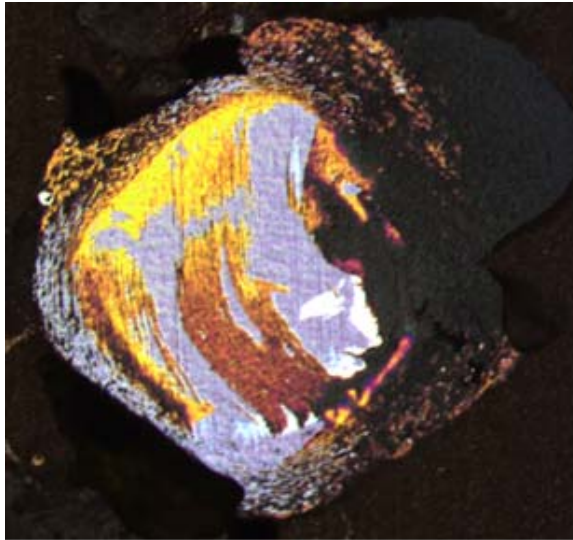
Typical load curve on a SCS4050 with 20 μm x 2 copper



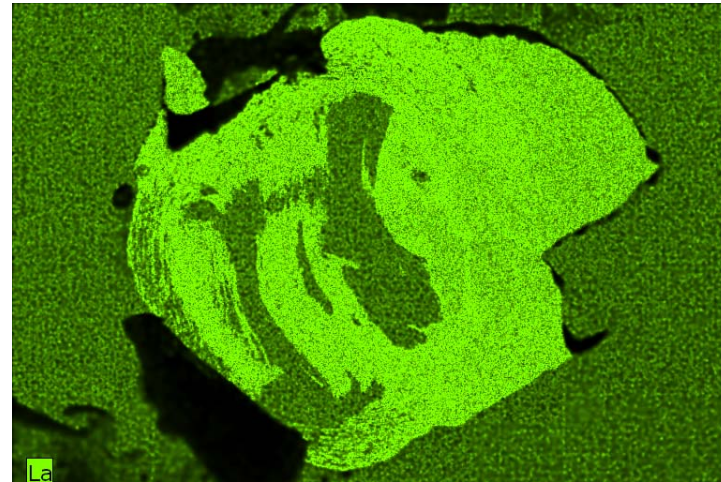
5 x Optical Image of the lower part of the multilayer structure after pull test clearly reveals a **debond zone** surrounded by a **dissipation zone**

- Local property at small region and small tensile force
- Informative features observed in load curve and the image of the delaminated region:
 - 1st peak load correspond to the debond of the multilayer structure; c-axis tensile strength can be derived using the debond zone area
 - 2nd peak load correspond to the tear off of top Cu stabilizer layer

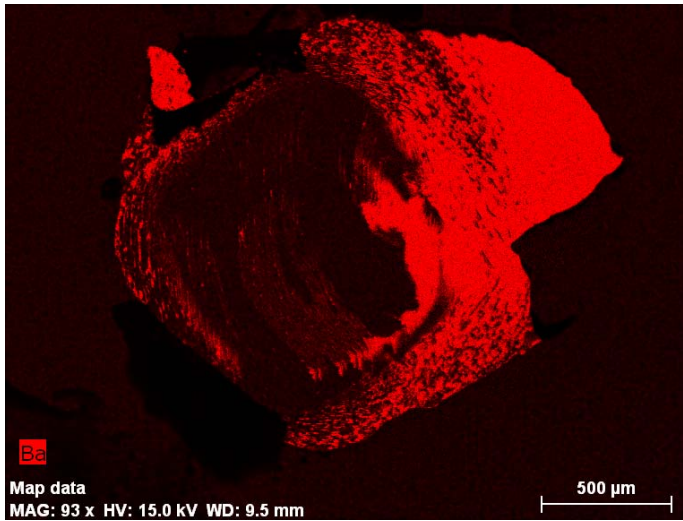
SEM-EDS study to identify delaminated interface



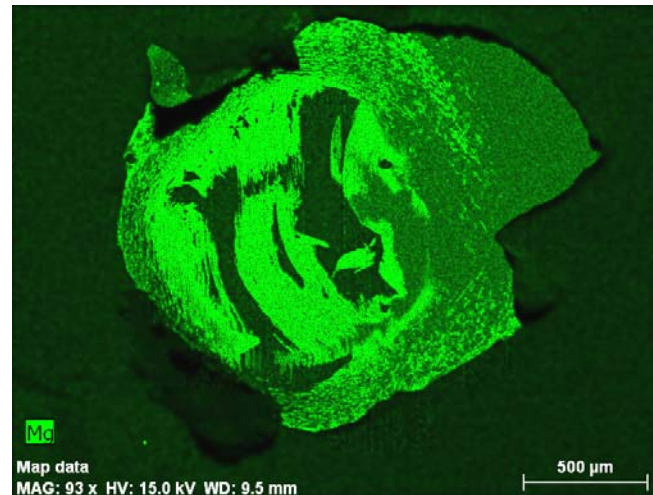
OM photo of delaminated region



EDS mapping - La

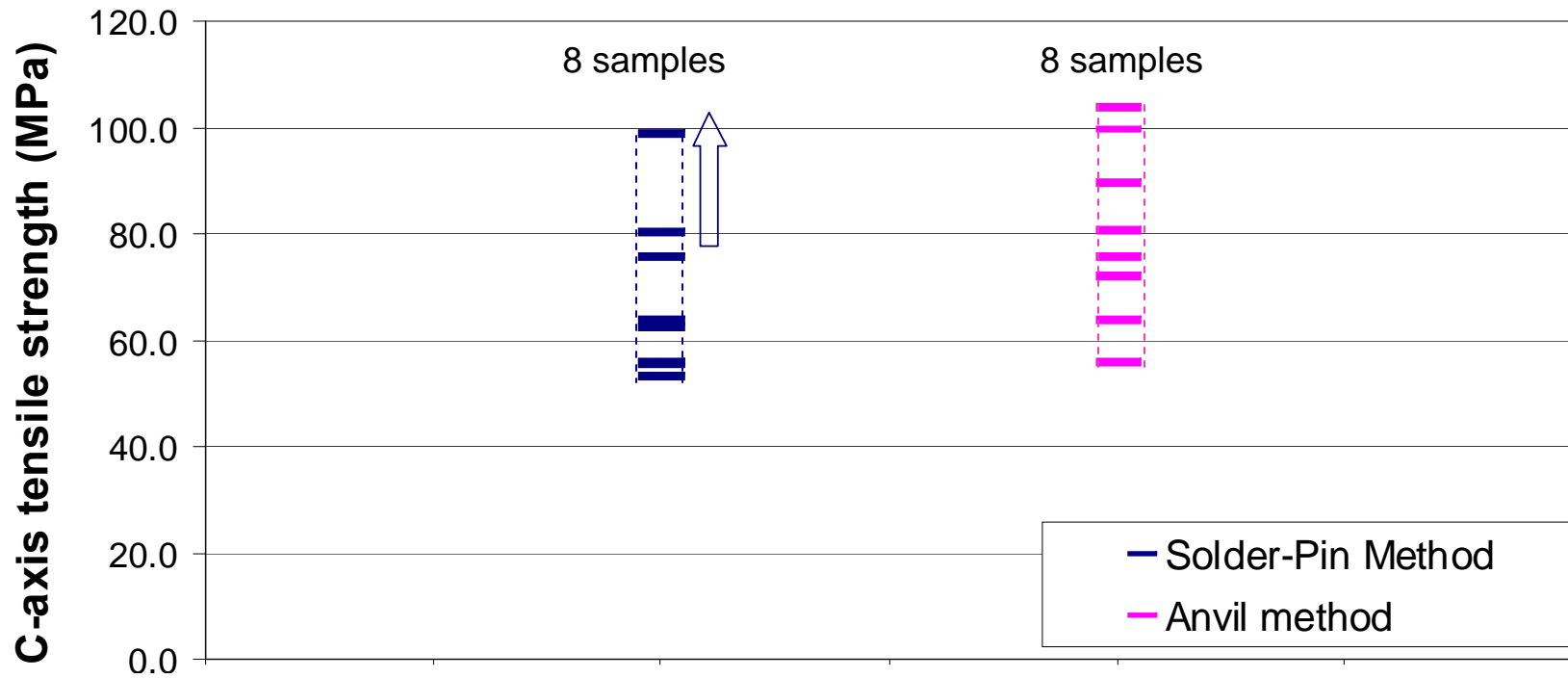


EDS mapping - Ba



EDS mapping - Mg

Test results on Wire 1 from two methods



C-axis tensile strength above 50 MPa and similar range of data points obtained from solder-pin method with test area of 1-2 mm² and anvil method with test area of 9-10 mm²

Conclusion

- Two methods of testing the c-axis tensile strength of 2G HTS are presented. The test results based on both methods show that there is some variation in c-axis tensile strength in 2G HTS while it can be as high as 100+ MPa
- The delamination regions from the c-axis pulling test reveal very informative features including debond zone and dissipation zone
- Interfaces at which delamination occurs at the peak load are exposed in the debond zone. Identifying those interface using OM and SEM-EDS and investigating their microstructure may help to find the reason for the variation of c-axis tensile strength in 2G HTS